PRODUCT/PROCESS
CHANGE NOTIFICATION

BCD5S 80V STANDARD DIFFUSION TRANSFER FROM CARROLLTON 6" TO ANG MO KIO 6"

Table 1. Change Implementation Schedule

| Forecasted implementation date for <br> change | 15 -Dec-2008 |
| :--- | :--- |
| Forecasted availabillity date of samples <br> for customer | $17-$ Oct-2008 |
| Forecasted date for STMicroelectronics <br> change Qualification Plan results availability | $17-$ Oct-2008 |
| Estimated date of changed product first <br> shipment | $05-$ Jan-2009 |

Table 2. Change Identification

| Related APCN | 3222 |
| :--- | :--- |
| Product Identification <br> (Product Family/Commercial Product) | ALL PRODUCTS IN THIS PROCESS TECHNOLOGY |
| Type of change | Waferfab location change |
| Reason for change | Restructuring plan as per Corporate CIL CRP/07/29/2900 <br> are transferring the process BCD5S 80V and related products <br> from Carrollton to AMK. |
| Description of the change |  |
|  |  |
| Product Line(s) and/or Part Number(s) |  |
| Description of the Qualification Plan |  |
| Change Product Identification |  |

Table 3. List of Attachments

| Customer Part numbers list |  |
| :--- | :--- |
| Qualification Plan results |  |




## DOCUMENT APPROVAL

| Name | Function |
| :---: | :---: |
| Pengo, Tullio | Division Marketing Manager |
| Cassani, Fabrizio | Division Product Manager |
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| Mervic, Alberto | Division Q.A. Manager |

## BCD5S 80V STANDARD DIFFUSION TRANSFER FROM CARROLLTON 6" TO ANG MO KIO 6"

WHAT:
Progressing along the Restructuring Plan already communicated by Corporate Information Letter (C.I.L.) CRP/07/2900 dated September 25, 2007 and APCN CRP/07/3222 dated December 28, 2007, please be informed that the products currently manufactured in Carrollton 6" Plant (Texas) by using BCD5 80V STANDARD Baseline Technology, will be moved to our facilities located in Ang Mo Kio 6" Plant (Singapore).

All the products manufactured by ST using BCD5 80V Baseline Technology, even if not expressly included in the above mentioned PIL \& APCN, are affected by this change.

WHY:
In order to optimize ST asset utilization and enhance performance for shareholders and customers.

## HOW:

By transferring and re-qualifying the mentioned front-end technology in the receiving plant; this technology has been qualified through a full set of evaluations on the selected test vehicle (TV for technology qualification): T84, EWS, electrical characterization, die and package oriented stress tests; others products diffused in the same Technology are qualified mainly by similarity (generic data) if assembled in the same package family. In case of different package families, stress test package oriented are carried on a "package test vehicle" (FE/BE compatibility) as listed in the annexed table.

| Techno family | Techno sub family | Product | Package | Product <br> Group | Qualification Plan |
| :--- | :--- | :---: | :---: | :---: | :---: |
| BCD5s 80V <br> Standard | BCD5s 80V <br> Standard | UK23 | Flexiwatt | APG | APG TV for technology <br> qualification |
|  |  | UK43 | PSO | APG | TV for FE/BE compatibility |

This transfer will not modify the electrical, dimensional and thermal parameters for the affected products, maintaining unchanged current information published on the relevant datasheets.
There is as well neither change in the packing modes nor in the standard delivery quantities either.
ST is focused on customer satisfaction in order to ensure a seamless transition in the supply of products from the new site.

## WHEN:

The production start and first shipments will be implemented according to our work in progress and materials availability. Full traceability is guaranteed by dedicated genealogy and traceability on the part.

We are ready to start shipments from AMK from mid December 08 onward.
The transfer of all product lines and the ramp up in the new location will be finalized within Q1 2009.

## Qualification program and results availability:

The relevant reliability reports of the test vehicles and process evaluation are provided below.

## Product's traceability:

Unless otherwise stated by customer specific requirement, new parts produced in AMK6 have a different traceability code as below:

| Diffusion plant | ID | Country of <br> origin |
| :---: | :---: | :---: |
| Carrollton <br> (current) | VH | Texas |
| AMK6 (new) | V6 | Singapore |

Shipments from new Wafer FAB location are tracked on the ST Standard Label as showed below :


## Samples availability:

Samples are available upon request to our local Sales Offices.

BCD5s 80V std family qualification approach

## XFER TO AMK6 <br> QUALIFICATION APPROACH

## The qualification plan was defined taking in account:

## Experience, Know how:

$\checkmark \quad$ The failure mode knowledge gained during the BCD past generation qualification.
$\checkmark \quad$ The experience gained during the BCD5 CST, AG, CF6 qualification.
Comparison between source and receiving plant in term of:
$\checkmark$ Process flow, Equipment, Data;
Procedures
$\checkmark \quad$ Internal ST (OP31).
$\checkmark \quad$ AEC Q100 Automotive qualification guideline.
The qualification has been obtained through a set of reliability investigation:
Construction Analysis,
$\checkmark \quad$ Wafer and Package Level Reliability
$\checkmark \quad$ Stress tests on elementary components
$\checkmark \quad$ Product Test Vehicle qualification for Silicon process qualification
$\checkmark \quad$ The Front End / Back End compatibility is evaluated through Package oriented test performed at Product Level.

## XFER TO AMK6 Analysis and Evaluation

|  | TEST | Stress condition | STRUCTURE | FAILURE MECHANISM |
| :---: | :---: | :---: | :---: | :---: |
| Investigation defined by Risk analysis. | HTS | 168hrs 250C | Metal 3 | Metal shunt resistance decrease |
|  |  |  | Contacts and Vias | Contacts and Vias instability |
|  | HTGS | 1000hrs 175C | 5V Pch | NBTI |
|  | HTRB |  | LDMOS PDMOS | Surface effects |
| Risk analysis based on know how and comparison between sending and receiving plant. | TDDB | - | Capacitors | Low Oxide Quality |
|  | Construction analysis | - | Struct. For CA | key features anomalies |
|  | JL3 + TC + DPA | JL3+1000TC | Product TV | IMD damage, metal displacement |
|  | JL3 + AC + DPA | JL3+AC | Product TV | corrosion |
|  | WBP and WBS | - | Product TV | Bonding weakness |
| Investigation defined by Q100 | Reported on the next slide |  |  |  |

## STRESS TEST ON PRODUCT TEST VEHICLES



## RELIABILITY REPORT

## TDA7563B Quad Power Amplifier

Author: Daniele Bini<br>Approved: Giacomo Burrone<br>Date: Castelletto, September $1^{\text {st }}, 2008$

[^0]
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## 1 RELIABILITY EVALUATION OVERVIEW

### 1.1 Objectives

The purpose of this document is to describe the reliability qualification trials, the results and the criteria used to evaluate the transfer of TDA7563B product line from CF6 to AMK6 plant.
The product is diffused in BCD5S technology and assembled in both PSO36 slug-up and FW27 packages.

### 1.2 Conclusion

The reliability tests performed on three lots of TDA7563B device diffused in BCD5S and assembled in FW27 package, gave the following results.

| HTOL | No failures and no significant drift on key parameters have been found after 1000h <br> of HTOL test |
| :--- | :--- |
| HTRB | No failures and no significant drift on key parameters have been found after 1000h <br> of HTRB test |
| HTSL | No failures have been found after 1000h of HTS test. |
| PTC | No failures and no significant drift on key parameters have been found after 1000c <br> of PTC test |
| THB | No failures have been found after preconditioning plus 1000h of THB test. |
| TC | No failures have been found after preconditioning plus 1000 thermal cycles. |
| AC | No failures have been found after preconditioning plus 96 hours of autoclave test. |
| ESD | HBM $\pm 2 k V$, MM $\pm 200 \mathrm{~V}$ and CDM $\pm 500 \mathrm{~V}$ were applied without failures. |
| LU | Injection current and over-voltage models were applied and no failures have been <br> detected. |

Moreover, the TDA7563B assembled in PSO36 package has to be considered qualified keeping into account the positive results obtained in the package oriented tests performed on TDA7575BPD product similar for functionality.

Therefore, considering

- The process is qualified and BCD5S products in AMK6 plant.
- The electrical characterization on TDA7563B device fulfills the product specification.

From the reliability point of view, the evaluation of TDA7563B devices has been positively completed.

## 2 DEVICE CHARACTERISTICS

### 2.1 Device description

## Features

- Multipower BCD technology
- MOSFET output power stage
- DMOS power output
- New Hi-efficiency (class SB)
- High output power capability $4 \times 28 \mathrm{~W} / 4 \Omega$ @ $14.4 \mathrm{~V}, 1 \mathrm{KHZ}, 10 \%$ THD, $4 \times 50 \mathrm{~W}$ max, power
- Max. output power $4 \times 72 \mathrm{~W} / 2 \Omega$
- Full $I^{2} \mathrm{C}$ bus driving:
- St-by
- Independent front/rear soft play/mute
- Selectable gain 30dB /16dB (for low noise line output function)
- High efficiency enable/disable
- $\mathrm{I}^{2} \mathrm{C}$ bus digital diagnostics (including DC bus AC load detection)
- Full fault protection
- DC offset detection
- Four independent short circuit protection
- Clipping detector pin with selectable threshold (2\%/10\%)
- St-by/mute pin
- Linear thermal shutdown with multiple thermal warning
- ESD protection


The TDA7563B is a new BCD technology Quad Bridge type of car radio amplifier in Flexiwatt27 package specially intended for car radio applications.
Thanks to the DMOS output stage the TDA7563B has a very low distortion allowing a clear powerful sound. Among the features, its superior efficiency performance coming from the internal exclusive structure, makes it the most suitable device to simplify the thermal management in high power sets.
The dissipated output power under average listening condition is in fact reduced up to $50 \%$ when compared to the level provided by conventional class AB solutions.

This device is equipped with a full diagnostics array that communicates the status of each speaker through the $\mathrm{I}^{2} \mathrm{C}$ bus.

### 2.2 Block Diagram



### 2.3 Construction note

### 2.3.1 Wafer fabrication information

|  | TDA7563B | TDA7563B | TDA7575B/ TDA7575BPD |
| :---: | :---: | :---: | :---: |
| Internal name: | UK23DC6 [UK23DD6] | UK23DB6 | UK43BC6 |
| Diffusion process: | BCD5S | BCD5S | BCD5S |
| Diffusion plant: | AMK | AMK | AMK |
| Wafer size [inches]: | $6{ }^{\prime \prime}$ | 6" | 6" |
| Wafer thickness [ $\mu \mathrm{m}$ ]: | 375 | 375 | 375 |
| Die sizes [ $\mathrm{mm}^{2}$ ]: | $6.00 \times 4.79$ | $6.00 \times 4.79$ | $3.75 \times 4.89$ |
| Passivation: | PSG+SiON+PIX | PSG+SiON+PIX | PSG+SiON+PIX |
| Back finishing: | $\mathrm{Cr} / \mathrm{Ni} / \mathrm{Au}$ | $\mathrm{Cr} / \mathrm{Ni} / \mathrm{Au}$ | $\mathrm{Cr} / \mathrm{Ni} / \mathrm{Au}$ |
| Pad Metallization[ $\mu \mathrm{m}$ ]: | $\begin{gathered} \text { AlSiCu: } \\ 0.4 \mathrm{~m}+0.8 \mathrm{um}+2.9 \mathrm{~mm} \end{gathered}$ | $\begin{gathered} \text { AISiCu: } \\ 0.4 u m+0.8 u m+2.9 u m \end{gathered}$ | $\begin{gathered} \text { AISiCu: } \\ 0.4 u m+0.8 u m+2.9 \mathrm{um} \end{gathered}$ |

### 2.3.2 Assembly information

| Package line: Assembly plant: Wires [mils]: | TDA7563B | TDA7575B/TDA7575BPD |
| :---: | :---: | :---: |
|  | FW27 | PSO36 |
|  | Malta | Muar |
|  | 2 mils, Cu | 3 mils, Au |
| Resin: | SUMITOMO 6300HW | HITACHI CEL 9240HF10 |
| Die Attach: | $\mathrm{Pb} / \mathrm{Ag} / \mathrm{Sn} 97.5 / 1.5 / 1$ | $\mathrm{Pb} / \mathrm{Ag} / \mathrm{Sn} 97.5 / 1.5 / 1$ |
| Frame Material | Cu | Cu |
| Lead Finishing: | Pure tin | Pure tin |

## 3 RELIABILITY TESTS RESULTS

| Test Name | Description | Purpose |
| :---: | :---: | :---: |
| HTOL | The device is stressed in dynamic configuration, approaching the operative max. ratings in terms of junction temperature, load current, internal power dissipation. | To simulate the worst-case application stress conditions. The typical failure modes are related to electromigration, wire-bonds degradation, oxide faults. |
| HTRB | The device is stressed in static configuration, approaching the absolute ratings in terms of junction temperature and supply voltage minimizing the power dissipation | To maximize the electrical field across either junctions or dielectric layers, in order to investigate the failure modes linked to mobile contamination, oxide ageing, and lay-out sensitivity to surface effects |
| ESD | The device is submitted to a high voltage peak on all his pins simulating ESD stress according to different simulation models. | To classify the device according to his susceptibility to damage or degradation by exposure to electrostatic discharge. |
| LU | The device is submitted to a direct current forced/sinked into the input/output pins. Removing the direct current no change in the supply current must be observed. | To verify the presence of bulk parasitic effect inducing latch-up. |
| PC | The device is submitted to a typical temperature profile used for surface mounting devices, after a controlled moisture absorption | As stand-alone test: to investigate the moisture sensitivity level. <br> As preconditioning before other reliability tests: to verify that the surface mounting stress does not impact on the subsequent reliability performance. <br> The typical failure modes are "pop corn" effect and delamination. |
| TC | The device is submitted to cycled temperature excursions, between a hot and a cold chamber in air atmosphere. | To investigate failure modes related to the thermo-mechanical stress induced by the different thermal expansion of the materials interacting in the die-package system. Typical failure modes are linked to metal displacement, dielectric cracking, molding compound delamination, wire-bonds failure, die-attach layer degradation. |
| $A C$ | The device is stored in saturated steam, at fixed and controlled conditions of pressure and temperature. | To investigate corrosion phenomena affecting die or package materials, related to chemical contamination and package hermeticity. |
| THB | The device is biased in static configuration minimizing its internal power dissipation, and stored at controlled conditions of ambient temperature and relative humidity | To evaluate the package moisture resistance with electrical field applied, both electrolytic and galvanic corrosion are put in evidence |


| Test Name | Description | Purpose |
| :---: | :---: | :---: |
| HTSL | The device is stored in unbiased condition at the <br> max. temperature allowed by the package <br> materials, sometimes higher than the max. <br> operative temperature | To investigate the failure mechanisms activated <br> by high temperature, typically wire-bonds solder <br> joint ageing, data retention faults, metal stress- <br> voiding |
| WBP | The wire is submitted to a pulling force <br> (approximately normal to the surface of the die) <br> able to achieve wire break or interface separation <br> between ball/pad or stitch/lead. | To investigate and measure the integrity and <br> robustness of the interface between wire and die <br> or lead metallization |
| WBS | The ball bond is submitted to a shear force <br> (parallel to the pad area) able to cause the <br> separation of the bonding surface between ball <br> bond and pad area. | To investigate and measure the integrity and <br> robustness of the bonding surface between ball <br> bond and pad area. |
| PTC | The device is stressed in dynamic configuration <br> approaching the operative conditions with an <br> alternate exposure at high and low temperature <br> extremes. | To simulate the actual combination of <br> environmental stresses interacting in the field <br> application. The typical failure modes are those <br> reported for HTOL and TC |

### 3.1 Reliability test plan and results summary

Here the tests plan and the results summary.

| Test | TDA7563B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | UK23DB | $\begin{aligned} & \text { UK23DC } \\ & \text { [UK23DD] } \end{aligned}$ |  |  |  |
|  | Conditions | Sample Size | Sample Size | Duration | Failure | Note |
| HTOL | $\begin{aligned} & \text { Vs }=16 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}, \\ & \text { Load }=2 \times[2 \Omega+300 \mu \mathrm{H}]+2 \times[4 \Omega+300 \mu \mathrm{H}] \end{aligned}$ | $77 \times 2$ lots | $77 \times 1$ lot | 1000h | 0 | - |
| HTRB | $\mathrm{Vs}=18 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, standby | $77 \times 2$ lots | - | 1000h | 0 | - |
| PTC | $\begin{aligned} & \text { Vs }=15 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}, \text { Load }=2 \times 2 \Omega \\ & \mathrm{Ta}=-40^{\circ} / 85^{\circ} \mathrm{C} \end{aligned}$ | $45 \times 1$ lot | - | 1000c | 0 | - |
| ELFR | Vs $=16 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, Load $=1.1 \mathrm{k} \Omega+22 \mu \mathrm{H}$ | $800 \times 3$ lots |  | 24h | 0 | - |
| ESD | $\mathrm{HBM} \pm 2 \mathrm{kV}[\mathrm{R}=1.5 \mathrm{k} \Omega, \mathrm{C}=100 \mathrm{pF}]$ | 6 | 6 | - | passed | - |
|  | MM $\pm 200 \mathrm{~V}[\mathrm{R}=0 \Omega, \mathrm{C}=200 \mathrm{pF}]$ | 6 | 6 | - | passed |  |
|  | $C D M \pm 500 \mathrm{~V}$ | 3 | 3 | - | passed |  |
| LU | Injection current ( Inom $\pm 100 \mathrm{~mA}$ ) | 6 | 6 | - | passed |  |
|  | Overvoltage (Vs 24 V ) | 4 | 4 | - | passed |  |
| HTSL | Ta $=+150^{\circ} \mathrm{C}$, unbiased | $45 \times 2$ lots | $\begin{gathered} 45 \times 1 \\ \text { lots } \end{gathered}$ | 1000h | 0 | - |
| THB | Vs $=18 \mathrm{~V}, \mathrm{Ta}=85^{\circ} \mathrm{C}, \mathrm{RH}=85 \%$, standby | $77 \times 2$ lots | $77 \times 1$ lot | 1000h | 0 | - |
| TC | $T a=-50^{\circ} \mathrm{C} /+150^{\circ} \mathrm{C}$ | $77 \times 2$ lots | $77 \times 1$ lot | 1000c | 0 | 1 |
| $A C$ | $\mathrm{Ta}=121^{\circ} \mathrm{C}, \mathrm{P}=2 \mathrm{~atm}$ | $77 \times 2$ lots | $77 \times 1$ lot | 96h | 0 | - |
| WBP | MIL STD883 Method 2011 | 30 bonds from a minimum of 5 devices |  | - | passed | 1 |
| WBS | AEC Q100-001 |  |  | - | passed | 1 |

1. WBP and WBS have been performed with positive results:

|  | Mean | Sigma | Min | Max |
| :--- | :---: | :---: | :---: | :---: |
| PULL TEST ON <br> VIRGIN PARTS | 52.4 | 4.0 | 45.0 | 59.0 |
| PULL TEST <br> AFTER TC | 33.6 | 5.4 | 18.5 | 43.5 |
| SHEAR TEST | 167.9 | 8.6 | 154 | 181 |


| Test | TDA7575BPD [UK43BC] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Conditions | Sample Size | Duration | Failure | Note |
| HTOL | $\begin{aligned} & \text { Vs }=16 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}, \\ & \text { Load (conf. 1) }=(1 \Omega+600 \mu \mathrm{H}) \\ & \text { Load (conf. 2) }=2 \times(2 \Omega+300 \mu \mathrm{H}) \end{aligned}$ | $77 \times 1$ lot | 1000h | 0 | - |
| HTRB | $\mathrm{Vs}=18 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, standby | $77 \times 1$ lot | 1000h | 0 | - |
| ESD | $\mathrm{HBM} \pm 2 \mathrm{kV}[\mathrm{R}=1.5 \mathrm{k} \Omega, C=100 \mathrm{pF}]$ | 6 | - | passed | - |
|  | $M M \pm 200 \mathrm{~V}[\mathrm{R}=0 \Omega, C=200 \mathrm{pF}]$ | 6 | - | passed |  |
|  | CDM $\pm 500 \mathrm{~V}$ | 3 | - | passed |  |
| LU | Injection current ( Inom $\pm 100 \mathrm{~mA}$ ) | 6 | - | passed |  |
|  | Overvoltage (Vs 24 V ) | 4 | - | passed |  |
| HTSL | Ta $=+150^{\circ} \mathrm{C}$, unbiased | $45 \times 1$ lot | 1000h | 0 | 3 |
| $\begin{gathered} \text { PC } \\ {[J L 3]} \end{gathered}$ | $\begin{aligned} & \text { BAKE: } 24 \mathrm{~h} \text { @ } 125^{\circ} \mathrm{C} \\ & \text { SOAK: } 192 \mathrm{~h} @ \mathrm{~T}=30^{\circ} \mathrm{C}, \mathrm{RH}=60 \% \\ & \text { REFLOW: } 3 \text { @ Tpeak } 245^{\circ} \mathrm{C} \end{aligned}$ | $250 \times 1$ lot | - | passed | 1 |
| THB | Vs $=18 \mathrm{~V}, \mathrm{Ta}=85^{\circ} \mathrm{C}, \mathrm{RH}=85 \%$, standby | $77 \times 1$ lot | 1000h | 0 | - |
| TC | $\mathrm{Ta}=-50^{\circ} \mathrm{C} /+150^{\circ} \mathrm{C}$ | $77 \times 1$ lot | 1000c | 0 | 2, 3 |
| $A C$ | $\mathrm{Ta}=121{ }^{\circ} \mathrm{C}, \mathrm{P}=2 \mathrm{~atm}$ | $77 \times 1$ lot | 96 h | 0 | - |
| WBP | MIL STD883 Method 2011 | 30 bonds from a | - | passed | 3 |
| WBS | AEC Q100-001 | minimum of 5 devices | - | passed | 3 |

1. No die delamination has been observed at SAM analysis after PC.
2. No die delamination has been observed after 1000 cycles.
3. WBP and WBS data:

|  | Mean | Sigma | Min | Max |
| :--- | :---: | :---: | :---: | :---: |
| PULL TEST <br> VIRGIN PARTS | 60.5 | 5.6 | 51.9 | 68.7 |
| PULL TEST <br> AFTER TC | 49.2 | 3.1 | 32.1 | 57.2 |
| PULL TEST <br> AFTER HTSL | 49.2 | 2.1 | 43.6 | 53.8 |
| SHEAR TEST | 263.4 | 12.1 | 247.3 | 279.2 |

## RELIABILITY REPORT

# TDA7575B [NDBA] PSO36 slug-up and FW27 packages 

Author: Daniele Bini<br>Approved: Giacomo Burrone<br>Date: Castelletto, August 11, 2008

[^1]
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## 1 RELIABILITY EVALUATION OVERVIEW

### 1.1 Objectives

The purpose of this document is to describe the reliability qualification trials, the results and the criteria used to evaluate the transfer of UK43 product line from CF6 to AMK6 plant.
The product is diffused in BCD5S technology and assembled in both PSO36 slug-up and FW27 packages.

### 1.2 Conclusion

The reliability tests performed on UK43BC (NDBA) device diffused in BCD5S and assembled in PowerSO36 package, gave the following results.

| HTOL | No failures and no significant drift on key parameters have been found after 1000h <br> of HTOL test |
| :--- | :--- |
| HTRB | No failures and no significant drift on key parameters have been found after 1000h <br> of HTRB test |
| HTSL | No failures have been found after 1000h of HTS test. |
| PC | No delamination has been observed after preconditioning sequence (JL3). |
| THB | No failures have been found after preconditioning plus 1000h of THB test. |
| TC | No failures have been found after preconditioning plus 1000 thermal cycles. |
| AC | No failures have been found after preconditioning plus 168 hours of autoclave test. |
| ESD | HBM $\pm 2 k V$, MM $\pm 200 \mathrm{~V}$ and CDM $\pm 500 \mathrm{~V}$ were applied without failures. |
| LU | Injection current and over-voltage models were applied and no failures have been <br> detected. |

Moreover, the UK43BC assembled in FW27 package has to be considered qualified keeping into account the positive results obtained in the package oriented tests performed on TDA7563B product similar for functionality but with a greater die-size ( $6.00 \times 4.79 \mathrm{~mm}$ ) see chapter three for details.

Therefore, considering

- The process is qualified and BCD5S products in AMK6 plant.
- The electrical characterization on UK43BC6 device fulfills the product specification.

From the reliability point of view, the evaluation of UK43BC6 devices has been positively completed.

## 2 DEVICE CHARACTERISTICS

### 2.1 Device description

■ DMOS POWER OUTPUT

- NON-SWITCHING HI-EFFICIENCY
- SINGLE-CHANNEL $1 \Omega$ DRIVING CAPABILITY
- HIGH OUTPUT POWER CAPABILITY $2 \times 28$ W/ $4 \Omega$ @ $14.4 \mathrm{~V}, 1 \mathrm{KHZ}, 10 \%$ THD, $2 \times 40 \mathrm{~W} / 4 \Omega$ EIAJ
- MAX. OUTPUT POWER $2 \times 75 \mathrm{~W} / 2 \Omega, 1 \times 150 \mathrm{~W} / 1 \Omega$
- SINGLE-CHANNEL $1 \Omega$ DRIVING CAPABILITY - 84W UNDISTORTED POWER
- FULL I ${ }^{2}$ C BUS DRIVING WITH 4 ADDRESS POSSIBILITIES:
- ST-BY, PLAY/MUTE, GAIN 12/26dB, FULL DIGITAL DIAGNOSTIC
- POSSIBILITY TO DISABLE THE I2C
- DIFFERENTAL INPUTS
- FULL FAULT PROTECTION
- DC OFFSET DETECTION
- TWO INDEPENDENT SHORT CIRCUIT PROTECTIONS
- CLIPPING DETECTOR PIN WITH SELECTABLE THRESHOLD (2\%/10\%)
■ ST-BY/MUTE PINS


## DESCRIPTION

The TDA7575 is a new BCD technology DUAL BRIDGE type of car radio amplifier in PowerSO36 and Flexiwatt27 packages specially intended for car radio applications. Thanks to the DMOS output stage

MULTIPOWER BCD TECHNOLOGY

the TDA7575 has a very low distortion allowing a clear powerful sound. Among the features, its superior efficiency performance coming from the internal exclusive structure, makes it the most suitable device to simplify the thermal management in high power sets. The dissipated output power under average listening condition is in fact reduced up to $50 \%$ when compared to the level provided by conventional class $A B$ solutions.
This device is equipped with a full diagnostic array that communicates the status of each speaker through the $\mathrm{I}^{2} \mathrm{C}$ bus. The TDA7575 has also the possibility of driving loads down to $1 \Omega$ paralleling the outputs into a single channel. It is also possible to disable the I2C and control the TDA7575 by means of the usual STBY and MUTE pins.

### 2.2 Block Diagram



### 2.3 Construction note

### 2.3.1 Wafer fabrication information

|  | TDA7575B/TDA7575BPD | TDA7563B |
| :---: | :---: | :---: |
| Internal name: <br> Diffusion process: | UK43BC6 | UK23DB6 |
|  | BCD5S | BCD5S |
| Diffusion plant: <br> Wafer size [inches]: | AMK | AMK |
|  | $6{ }^{\prime \prime}$ | $6{ }^{\prime \prime}$ |
| Wafer thickness [ $\mu \mathrm{m}$ ]: | 375 | 375 |
| Die sizes [ $\mathrm{mm}^{2}$ ]: | $3.75 \times 4.89$ | $6.00 \times 4.79$ |
| Passivation: Back finishing: | PSG+SiON+PIX | PSG+SiON+PIX |
|  | $\mathrm{Cr} / \mathrm{Ni} / \mathrm{Au}$ | $\mathrm{Cr} / \mathrm{Ni} / \mathrm{Au}$ |
| Pad Metallization[ $\mu \mathrm{m}$ ]: | AlSiCu: $0.4 \mathrm{um}+0.8 \mathrm{um}+2.9 \mathrm{um}$ | AlSiCu: $0.4 \mathrm{um}+0.8 \mathrm{um}+2.9 \mathrm{um}$ |

### 2.3.2 Assembly information

|  | TDA7575B/TDA7575BPD | TDA7563B |
| :---: | :---: | :---: |
| Package line: | PSO36 | FW27 |
| Assembly plant: | Muar | Malta |
| Wires [mils]: | 3 mils, Au | 2 mils, Cu |
| Resin: | HITACHI CEL 9240HF10 | SUMITOMO 6300HW |
| Die Attach: | $\mathrm{Pb} / \mathrm{Ag} / \mathrm{Sn} 97.5 / 1.5 / 1$ | $\mathrm{Pb} / \mathrm{Ag} / \mathrm{Sn} 97.5 / 1.5 / 1$ |
| Frame Material | Cu | Cu |
| Lead Finishing: | Pure tin | Pure tin |

## 3 RELIABILITY TESTS RESULTS

| Test Name | Description | Purpose |
| :---: | :---: | :---: |
| HTOL | The device is stressed in dynamic configuration, approaching the operative max. ratings in terms of junction temperature, load current, internal power dissipation. | To simulate the worst-case application stress conditions. The typical failure modes are related to electromigration, wire-bonds degradation, oxide faults. |
| HTRB | The device is stressed in static configuration, approaching the absolute ratings in terms of junction temperature and supply voltage minimizing the power dissipation | To maximize the electrical field across either junctions or dielectric layers, in order to investigate the failure modes linked to mobile contamination, oxide ageing, and lay-out sensitivity to surface effects |
| ESD | The device is submitted to a high voltage peak on all his pins simulating ESD stress according to different simulation models. | To classify the device according to his susceptibility to damage or degradation by exposure to electrostatic discharge. |
| LU | The device is submitted to a direct current forced/sinked into the input/output pins. Removing the direct current no change in the supply current must be observed. | To verify the presence of bulk parasitic effect inducing latch-up. |
| PC | The device is submitted to a typical temperature profile used for surface mounting devices, after a controlled moisture absorption | As stand-alone test: to investigate the moisture sensitivity level. <br> As preconditioning before other reliability tests: to verify that the surface mounting stress does not impact on the subsequent reliability performance. <br> The typical failure modes are "pop corn" effect and delamination. |
| TC | The device is submitted to cycled temperature excursions, between a hot and a cold chamber in air atmosphere. | To investigate failure modes related to the thermo-mechanical stress induced by the different thermal expansion of the materials interacting in the die-package system. Typical failure modes are linked to metal displacement, dielectric cracking, molding compound delamination, wire-bonds failure, die-attach layer degradation. |
| $A C$ | The device is stored in saturated steam, at fixed and controlled conditions of pressure and temperature. | To investigate corrosion phenomena affecting die or package materials, related to chemical contamination and package hermeticity. |
| THB | The device is biased in static configuration minimizing its internal power dissipation, and stored at controlled conditions of ambient temperature and relative humidity | To evaluate the package moisture resistance with electrical field applied, both electrolytic and galvanic corrosion are put in evidence |


| Test Name | Description | Purpose |
| :---: | :---: | :---: |
| HTSL | The device is stored in unbiased condition at the <br> max. temperature allowed by the package <br> materials, sometimes higher than the max. <br> operative temperature | To investigate the failure mechanisms activated <br> by high temperature, typically wire-bonds solder <br> joint ageing, data retention faults, metal stress- <br> voiding |
| WBP | The wire is submitted to a pulling force <br> (approximately normal to the surface of the die) <br> able to achieve wire break or interface separation <br> between ball/pad or stitch/lead. | To investigate and measure the integrity and <br> robustness of the interface between wire and die <br> or lead metallization |
| WBS | The ball bond is submitted to a shear force <br> (parallel to the pad area) able to cause the <br> separation of the bonding surface between ball <br> bond and pad area. | To investigate and measure the integrity and <br> robustness of the bonding surface between ball <br> bond and pad area. |
| PTC | The device is stressed in dynamic configuration <br> approaching the operative conditions with an <br> alternate exposure at high and low temperature <br> extremes. | To simulate the actual combination of <br> environmental stresses interacting in the field <br> application. The typical failure modes are those <br> reported for HTOL and TC |

### 3.1 Reliability test plan and results summary

Here the tests plan and the results summary.

| Test | TDA7575BPD |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Conditions | Sample Size | Duration | Failure | Note |
| HTOL | $\begin{aligned} & \text { Vs=16V, Tj=150 }{ }^{\circ} \mathrm{C}, \\ & \text { Load (conf. 1) }=(1 \Omega+600 \mu \mathrm{H}) \\ & \text { Load (conf. 2) }=2 \times(2 \Omega+300 \mu \mathrm{H}) \end{aligned}$ | $77 \times 1$ lot | 1000h | 0 | - |
| HTRB | $\mathrm{Vs}=18 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, standby | $77 \times 1$ lot | 1000h | 0 | - |
| ESD | $\mathrm{HBM} \pm 2 \mathrm{kV}[\mathrm{R}=1.5 \mathrm{k} \Omega, C=100 \mathrm{pF}]$ | 6 | - | passed | - |
|  | $M M \pm 200 \mathrm{~V}[\mathrm{R}=0 \Omega, \mathrm{C}=200 \mathrm{pF}]$ | 6 | - | passed |  |
|  | CDM $\pm 500 \mathrm{~V}$ | 3 | - | passed |  |
| LU | Injection current ( Inom $\pm 100 \mathrm{~mA}$ ) | 6 | - | passed |  |
|  | Overvoltage (Vs 24 V ) | 4 | - | passed |  |
| HTSL | Ta $=+150^{\circ} \mathrm{C}$, unbiased | $45 \times 1$ lot | 1000h | 0 | 3 |
| $\begin{gathered} \text { PC } \\ {[J L 3]} \end{gathered}$ | $\begin{aligned} & \text { BAKE: } 24 \mathrm{~h} \text { @ } 125^{\circ} \mathrm{C} \\ & \text { SOAK: } 192 \mathrm{~h} @ \mathrm{~T}=30^{\circ} \mathrm{C}, \mathrm{RH}=60 \% \\ & \text { REFLOW: } 3 \text { @ Tpeak }=245^{\circ} \mathrm{C} \end{aligned}$ | $250 \times 1$ lot | - | passed | 1 |
| THB | Vs $=18 \mathrm{~V}, \mathrm{Ta}=85^{\circ} \mathrm{C}, \mathrm{RH}=85 \%$, standby | $77 \times 1$ lot | 1000h | 0 | - |
| TC | Ta $=-50^{\circ} \mathrm{C} /+150^{\circ} \mathrm{C}$ | $77 \times 1$ lot | 1000c | 0 | 2,3 |
| $A C$ | $\mathrm{Ta}=121^{\circ} \mathrm{C}, \mathrm{P}=2 \mathrm{~atm}$ | $77 \times 1$ lot | 96h | 0 | - |
| WBP | MIL STD883 Method 2011 | 30 bonds from a | - | passed | 3 |
| WBS | AEC Q100-001 | minimum of 5 devices | - | passed | 3 |

1. No die delamination has been observed at SAM analysis after PC.
2. No die delamination has been observed after 1000 cy .
3. WBP data

|  | Mean | Sigma | Min | Max |
| :--- | :---: | :---: | :---: | :---: |
| PULL TEST <br> AFTER TC | 49.2 | 3.1 | 32.1 | 57.2 |
| PULL TEST <br> AFTER HTSL | 49.2 | 2.1 | 43.6 | 53.8 |


| Test | TDA7563B |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Conditions | Sample Size | Duration | Failure | Note |
| HTOL | $\begin{aligned} & \text { Vs }=16 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}, \\ & \text { Load }=2 \times[2 \Omega+300 \mu \mathrm{H}]+2 \times[4 \Omega+300 \mu \mathrm{H}] \end{aligned}$ | $77 \times 2$ lots | 1000h | 0 | - |
| HTRB | $\mathrm{Vs}=18 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, standby | $77 \times 2$ lots | 1000h | 0 | - |
| PTC | $\begin{aligned} & \text { Vs }=15 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}, \text { Load }=2 \times 2 \Omega \\ & \mathrm{Ta}=-40^{\circ} / 85^{\circ} \mathrm{C} \end{aligned}$ | $45 \times 1$ lot | 1000c | 0 | - |
| ELFR | Vs $=16 \mathrm{~V}, \mathrm{Tj}=150^{\circ} \mathrm{C}$, Load $=1 \mathrm{k} \Omega+22 \mu \mathrm{H}$ | $800 \times 2$ lots | 24h | 0 | - |
| ESD | $\mathrm{HBM} \pm 2 \mathrm{kV}[\mathrm{R}=1.5 \mathrm{k} \Omega, \mathrm{C}=100 \mathrm{pF}]$ | 6 | - | passed | - |
|  | $M M \pm 200 \mathrm{~V}[\mathrm{R}=0 \Omega, \mathrm{C}=200 \mathrm{pF}]$ | 6 | - | passed |  |
|  | $C D M \pm 500 \mathrm{~V}$ | 3 | - | passed |  |
| LU | Injection current ( Inom $\pm 100 \mathrm{~mA}$ ) | 6 | - | passed |  |
|  | Overvoltage (Vs 24 V ) | 4 | - | passed |  |
| HTSL | Ta $=+150^{\circ} \mathrm{C}$, unbiased | $77 \times 2$ lots | 1000h | 0 | - |
| THB | Vs=18V, $\mathrm{Ta}=85^{\circ} \mathrm{C}, \mathrm{RH}=85 \%$, standby | $77 \times 2$ lots | 1000h | 0 | - |
| TC | $\mathrm{Ta}=-50^{\circ} \mathrm{C} /+150^{\circ} \mathrm{C}$ | $77 \times 2$ lots | 1000c | 0 | 1 |
| $A C$ | $\mathrm{Ta}=121^{\circ} \mathrm{C}, \mathrm{P}=2 \mathrm{~atm}$ | $77 \times 2$ lots | 96h | 0 | - |
| WBP | MIL STD883 Method 2011 | 30 bonds from a minimum of 5 devices | - | passed | 1 |
| WBS | AEC Q100-001 |  | - | passed | 1 |

1. WBP have been performed with positive results:

|  | Mean | Sigma | Min | Max |
| :--- | :---: | :---: | :---: | :---: |
| PULL TEST ON <br> VIRGIN PARTS | 52.4 | 4.0 | 45.0 | 59.0 |
| PuLL TEST <br> AFTER TC | 33.6 | 5.4 | 18.5 | 43.5 |
| SHEAR TEST | 167.9 | 8.6 | 154 | 181 |

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